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AN INVESTIGATION INTO THE HYPERGOLICITY OF DICYANAMIDE-BASED IONIC LIQUID

FUELS WITH COMMON OXIDIZERS (PREPRINT)

E. Dambach and S. Heister
Purdue University – Aeronautics and Astronautics
West Lafayette, IN

I. Ismail, S. Schneider, and T. Hawkins Air Force Research Laboratory Edwards Air Force Base, CA

ABSTRACT

Previous studies have demonstrated that substituted imidazolium dicyanamides are hypergolic with nitric acid. An investigation was conducted to study the hypergolicity of selected dicyanamides, commercially available 1-butyl-3-methyl-imidazolium dicyanamide and Air Force Research Laboratory developed AF-IL-617, with common oxidizers. Diluents, particularly water and methanol, were introduced to the fuel in an effort to understand the effect on the ignition delay. The water dilution limit at which ignition would still occur was obtained for the two dicyanamide-based fuels with white fuming nitric acid. Controlled droplet experiments were conducted with high speed photography at 1040 frames per second to establish the ignition delays.

INTRODUCTION

The current state-of-the-art in hypergolic bipropellant technology is monomethyl hydrazine (MMH) and nitrogen tetroxide (NTO, N₂O₄). Both are highly toxic and difficult to handle, which has lead to a push for "greener" propellants. Ionic liquids, which are defined as salts with a melting point below the boiling point of water, possess qualities that if adequate performance can be attained could prove to be suitable replacements. These properties include: low melting point, low to negligible vapor pressure, long liquid range, high thermal stability, and high density. Adequate performance is defined as having a superior density impulse and an ignition delay comparable to that of the state-of-the-art. A long ignition delay is unfavorable because it allows for the accumulation of explosive intermediate species that may detonate upon ignition (hard engine start). A previous study performed by the Air Force Research Laboratory identified a class of ionic liquids containing the dicyanamide anion to be hypergolic with common oxidizer, nitric acid.² The focus of the study was to investigate the hypergolicity of dicyanamidebased fuels with common oxidizers, in an effort to identify hypergolic propellant combinations and measure ignition delay times comparable to that of hydrazine and its derivatives. The key objectives were as follows: use drop testing as a screening tool to study the hypergolicity of ionic liquid dicyanamide-based fuels with common oxidizers and obtain ignition delay times; obtain precise fuel droplet volume measurements through the use of a remote-controlled metered droplet release; and study effect of diluting dicyanamide-based fuels with protonic agents (water and methanol) on hypergolicity.

EXPERIMENTAL FACILITY

A single run consisted of dispensing a small droplet of fuel into a cuvette with typically 250 μ L or 500 μ L of oxidizer. The bulk of the testing focused upon two work-horse dicyanamide-based fuels: 1-butyl-3-methyl-imidazolium dicyanamide (BMIMDCA) and AF-IL-617. BMIMDCA

is commercially available, and AF-IL-617 was developed in-house at AFRL. The oxidizers of interest were white fuming nitric acid (WFNA), hydroxylammonium nitrate (HAN) [82% HAN and S. HAN 5], nitrogen tetroxide, and 93% hydrogen peroxide (H_2O_2). The following mini-ignition studies were conducted: test BMIMDCA and AF-IL-617 with WFNA, test BMIMDCA and AF-IL-617 with HAN; establish water dilution limit of BMIMDCA and AF-IL-617 with WFNA; obtain data points for methanol-diluted samples of BMIMDCA and AF-IL-617 with WFNA, investigate water-dilution of WFNA with BMIMDCA and AF-IL-617; test AF-IL-617 with NTO; test AF-IL-617 with H_2O_2 ; establish baseline using H_2O_2 and H_2O_2 and H_3O_2 and H_3O_2

The experiment utilized a Harvard Apparatus Nanomite Syringe Pump with a 10 μ L glass hypodermic syringe to dispense the fuel droplet into the pool of oxidizer in a cuvette 4.6 cm below. The drop test was recorded at 1040 fps with a monochrome IDT Redlake MotionPro X3 High Speed Digital Camera. Refer to Figure 1 and Figure 2 to see the complete test set-up.





Figure 1. Test Set-up

Figure 2. Test Set-up within Ventilation Hood

For each run, the droplet volume and the ignition delay were measured. For one person to conduct the tests independently, it was not possible to observe the actual droplet volume and trigger the high speed camera at the same time. In order to obtain an understanding of the droplet volume, test drops into water were conducted with the fuel prior to introducing the oxidizer to the cuvette. For each test drop, at the moment that the droplet was released from the syringe tip, the metering pump was stopped with the foot pedal and the volume displayed on the control unit was recorded. This process was typically repeated three to five times. The measurements proved to be quite precise the majority of the time, and the volumes were averaged to obtain the reported droplet volume. The average fuel droplet size was 6.7 μ L with a standard deviation of 1.0 μ L, which corresponds to a droplet diameter on the order of 2 mm. The uncertainty associated with these measurements was 0.5 μ L. See Figure 3 for a picture of the droplet on the syringe tip.

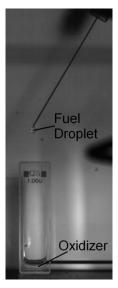


Figure 3. Fuel Droplet on Tip of Syringe

The ignition delay time was obtained by finding the difference in time between the fuel and oxidizer mixing and ignition. Fuel and oxidizer contact was defined as the frame when the fuel droplet was first completely immersed in the oxidizer. Ignition was defined as the frame when the flash was first visible. One frame corresponded to the passage of 0.96 ms. The uncertainty of these measurements was one frame. Refer to Figure 4 for a picture of fuel and oxidizer contact and Figure 5 for a picture of ignition.



Figure 4. Fuel and Oxidizer Mix



Figure 5. Ignition

RESULTS AND DISCUSSION

Over 100 droplet tests were conducted throughout the study. Table 1 summarizes whether or not ignition occurred for each of the propellant combinations. Figure 6 and Figure 7 show the effect on the ignition delay of diluting BMIMDCA and AF-IL-617 with water or methanol, as well as the measured ignition delays for hydrazine and MMH.

Table 1. Summary of Ignition Events

Fuel	Oxidizer	Ignition?
BMIMDCA	WFNA	Yes
BMIMDCA	WFNA / ≥4% H ₂ O	No
BMIMDCA	82% HAN	No
BMIMDCA	S. HAN 5	No
BMIMDCA / ≤19.5% H ₂ O	WFNA	Yes
BMIMDCA / ≥20% H ₂ O	WFNA	No
BMIMDCA / ≤17.8% MeOH*	WFNA	Yes
AF-IL-617	WFNA	Yes
AF-IL-617	WFNA / ≤10.2% H ₂ O	Yes
AF-IL-617	WFNA / ≥13.7% H ₂ O	No
AF-IL-617	82% HAN	No
AF-IL-617	S. HAN 5	No
AF-IL-617	93% H ₂ O ₂	No
AF-IL-617 / ≤22.2% H ₂ O	WFNA	Yes
AF-IL-617 / ≥24.4% H ₂ O	WFNA	No
AF-IL-617 / ≤18.6% MeOH*	WFNA	Yes
AF-IL-617 / 10% H ₂ O	N_2O_4	No
AF-IL-617 / 25.2% H ₂ O	N_2O_4	No
MeOH	WFNA	No

^{*}This was the highest concentration of methanol attempted and does not represent a dilution limit.

The survey provided insight as to what propellant combinations were hypergolic. As was previously discussed, the dicyanamide-based fuels proved to be hypergolic with nitric acid. AF-IL-617 diluted with water was attempted with nitrogen tetroxide because the hypothesis was that the water in the fuel would react with the nitrogen tetroxide and form nitric acid, which in turn, would react with the fuel and ignite the mixture. Unfortunately, this did not prove fruitful during the brief study. The reactions, though, were quite violent and appeared to be very close to the point of igniting. On the contrary, dropping AF-IL-617 into HAN or $93\%~H_2O_2$ proved unexciting, as no reaction was observed.

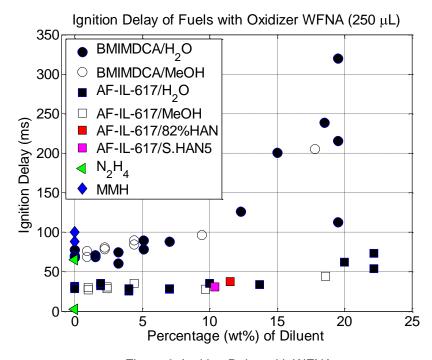


Figure 6. Ignition Delay with WFNA

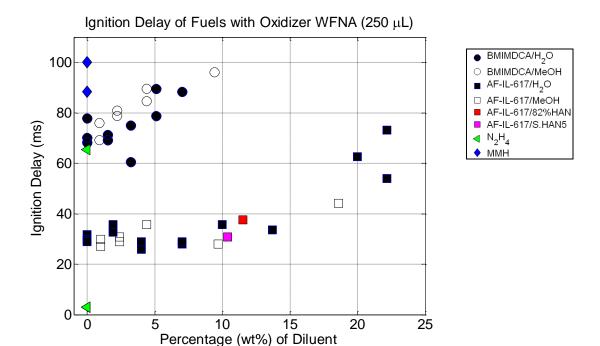


Figure 7. Ignition Delay with WFNA (zoomed)

By adding water or methanol to BMIMDCA, the ignition delay appeared to increase steadily, almost exponentially. On the other hand, the addition of a diluent (below 14% of the total mass) to AF-IL-617 did not affect the ignition delay much. Also, at low concentrations of diluent, the ignition delays of the dicyanamides were repeatable. In contrast, increasing the concentration of the diluent decreased the repeatability of the experiment, as was evident by the BMIMDCA/19.5% H₂O case. Most likely, this was a result of inadequate mixing of the fuel and the diluent. Droplets of diluent were dispensed into the fuel, and then the fuel and diluent solution was swirled in a small vial; for the cases where there was a large concentration of diluent, it was quite possible that the fuel and diluent did not mix fully. Of the pure fuels, MMH has the highest ignition delay with hydrazine having the greatest variation. The combustion reaction of hydrazine and WFNA involves no carbon and generates no visible flame. The lack of a visible flame made it difficult to infer the ignition delay time for the reaction.

Figures 8 through Figure 12 show the theoretical performance of the propellant combinations of the fuels BMIMDCA, AF-IL-617, hydrazine, and MMH with oxidizer WFNA. The calculations were performed using the NASA Thermochemistry code³ assuming a chamber pressure of 152 psia and an expansion area ratio of 22. The conditions correspond to the MMH/NTO primary reaction control thrusters onboard the Space Shuttle.⁴ The values represented in Figure 8, Figure 9, Figure 11, and Figure 12 correspond to the mixture ratio that maximizes the vacuum specific impulse (BMIMDCA O/F = 3.2, AF-IL-617 O/F = 2.5, N_2H_4 O/F = 1.5, and MMH O/F = 2.6), where as in Figure 10, the characteristic velocity was optimized (BMIMDCA O/F = 2.6, AF-IL-617 O/F = 1.9, N_2H_4 O/F = 1.3, and MMH O/F = 2.1).

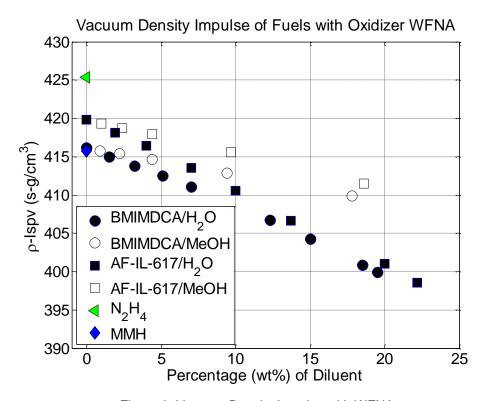


Figure 8. Vacuum Density Impulse with WFNA

As expected, with the addition of a diluent to the fuel, the performance decreased. Hydrazine proved to be superior to AF-IL-617. On the contrary, MMH is the state-of-the-art hypergolic fuel in use, and AF-IL-617 can be diluted down to 95% and maintain comparable, if not, superior performance. The density specific impulse of MMH/NTO is lower than that of AF-IL-617/WFNA at 412 s-g/cm³ under the same conditions with a mixture ratio of 2.2. As observed in Figure 9 and Figure 10, the vacuum specific impulses and characteristic velocities of the dicyanamide-based fuels were significantly lower than the hydrazine fuels. The vacuum specific impulse of 328 s and the characteristic velocity of 1740 m/s for MMH/NTO far exceeded the corresponding values of the other propellant combinations.

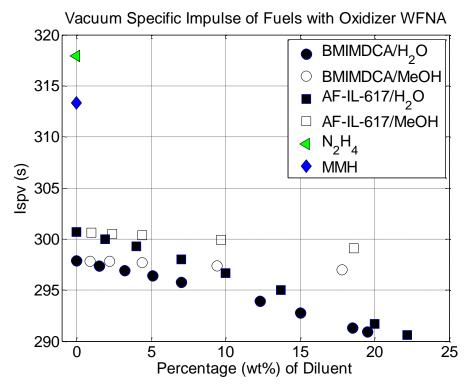


Figure 9. Vacuum Specific Impulse with WFNA

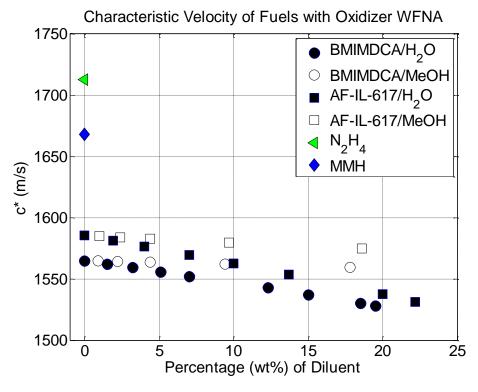


Figure 10. Characteristic Velocity with WFNA

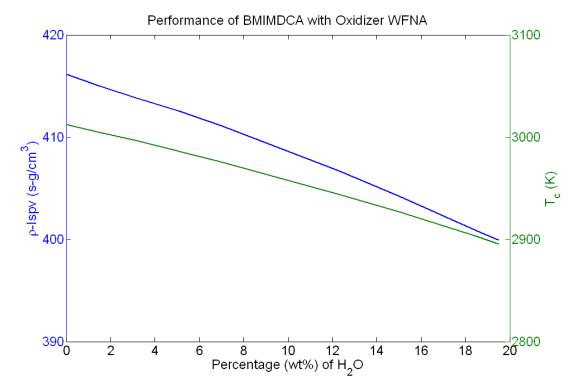


Figure 11. Effect of H₂O on BMIMDCA Performance with WFNA

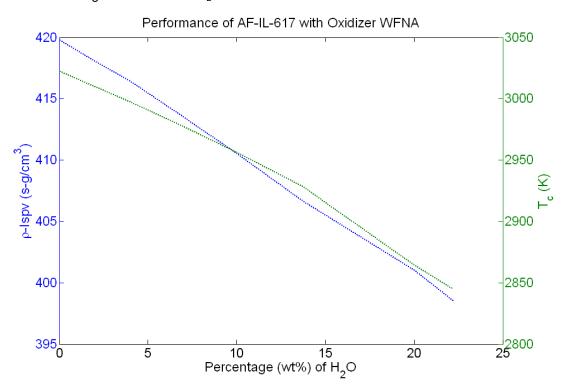


Figure 12. Effect of H₂O on AF-IL-617 Performance with WFNA

One of the concerns involving ionic liquids is the high flame temperatures experienced during combustion. The addition of water to the fuel effectively decreased the temperatures to levels comparable to that of hydrazine (2900 K) and MMH (2970 K).

Figure 13 represents the effect of the mixture ratio on the ignition delay. An average mixture ratio was calculated for each of the fuel and particular volumes of WFNA. As one would expect, by doubling the volume of the oxidizer, the value of the mixture ratio would also double. This was not the case for BMIMDCA. The fuel droplet volumes for one of the BMIMDCA / 250 μL WFNA cases and the BMIMDCA / 500 μL WFNA case were approximately half that of the other two BMIMDCA / 250 μL WFNA cases, which resulted in the skewed average O/F of 67 relative to 190.

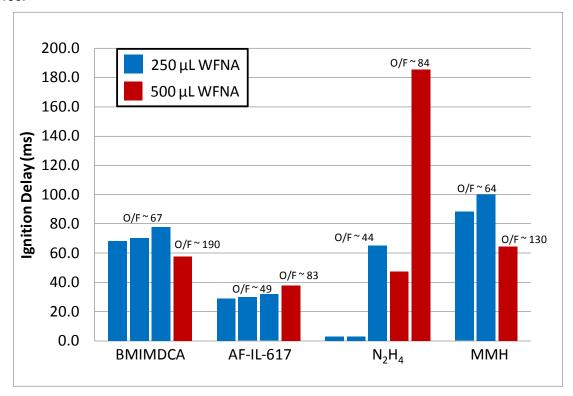


Figure 13. Effect of O/F on Ignition Delay

Obviously, the mixture ratios experienced during the droplet testing are far from optimal. The mixture ratios that maximize the vacuum specific impulse as described above are reproduced here for convenience as follows for the respective fuels: BMIMDCA O/F = 3.2, AF-IL-617 O/F = 2.5, N_2H_4 O/F = 1.5, and MMH O/F = 2.6.

SUMMARY AND CONCLUSIONS

The syringe metering pump was utilized to remotely and precisely dispense fuel droplets for over one hundred hypergolic droplet tests. The hypergolicity of BMIMDCA and AF-IL-617 with WFNA was established but not with HAN or $93\%\ H_2O_2$. The H_2O dilution limit for BMIMDCA was between 19.5% and 20%. With increasing concentration of diluent (H_2O or MeOH), the ignition delay of BMIMDCA and WFNA increased steadily from ~70 ms. The H_2O dilution limit for AF-IL-617 was between 22.2% and 24.4%. Below 14% diluent (H_2O or MeOH), the ignition delay of AF-IL-617 and WFNA remained around 30 ms. BMIMDCA will not ignite with 96% WFNA, where as AF-IL-617 will still ignite with 90% WFNA. As mentioned previously, hypergolic drop tests are only screening tools for new propellants. The acceptable delay time is not known and is highly dependent on the experimental configuration or the thruster, injector and plumbing design. It is important to note that the ignition delays for both BMIMDCA and AF-IL-617 were of the same order of magnitude of the baseline cases with hydrazine and MMH. The results involving AF-IL-617 are highly encouraging and necessitate further study.

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